

3-1-2020

Effect of Fiber Reinforced Polymer Tubes Filled with Recycled Materials and Concrete on Structural Capacity of Pile Foundations

Visar Farhangi

University of Nevada, Las Vegas, farhangi@unlv.nevada.edu

Moses Karakouzian

University of Nevada, Las Vegas, moses.karakouzian@unlv.edu

Follow this and additional works at: https://digitalscholarship.unlv.edu/fac_articles



Part of the [Civil and Environmental Engineering Commons](#)

Repository Citation

Farhangi, V., Karakouzian, M. (2020). Effect of Fiber Reinforced Polymer Tubes Filled with Recycled Materials and Concrete on Structural Capacity of Pile Foundations. *Applied Sciences*, 10(5), 1-14. <http://dx.doi.org/10.3390/app10051554>

This Article is protected by copyright and/or related rights. It has been brought to you by Digital Scholarship@UNLV with permission from the rights-holder(s). You are free to use this Article in any way that is permitted by the copyright and related rights legislation that applies to your use. For other uses you need to obtain permission from the rights-holder(s) directly, unless additional rights are indicated by a Creative Commons license in the record and/or on the work itself.

This Article has been accepted for inclusion in Civil & Environmental Engineering and Construction Faculty Publications by an authorized administrator of Digital Scholarship@UNLV. For more information, please contact digitalscholarship@unlv.edu.

Article

Effect of Fiber Reinforced Polymer Tubes Filled with Recycled Materials and Concrete on Structural Capacity of Pile Foundations

Visar Farhangi *  and Moses Karakouzian 

Department of Civil and Environmental Engineering and Construction, University of Nevada, Las Vegas, NV 89154, USA; mkar@unlv.nevada.edu

* Correspondence: farhangi@unlv.nevada.edu

Received: 4 February 2020; Accepted: 21 February 2020; Published: 25 February 2020



Abstract: This paper deals with analyzing the structural responses of glass-fiber-reinforced polymer (GFRP) tubes filled with recycled and concrete material for developing composite piles, as an alternative to traditional steel reinforced piles in bridge foundations. The full-scale GFRP composite piles included three structural layers, using a fiber-oriented material that was inclined longitudinally. Almost 60% of the fibers were orientated at 35° from the longitudinal direction of the pile and the rest 40 percent were oriented at 86° from the horizontal axis. The segment between the inner and outer layers was inclined 3° from the hoop direction in the tube. The behavior of the filled GFRP tubes was semi-linear and resulted in increasing the total ductility and strength of the piles. Adjusting the material's properties, such as the E_{Axial} , E_{Hoop} , and Poisson ratios, optimized the results. The lateral strength of the GFRP composite pile and pre-stressed piles are investigated under both axial compression and bending moment loads. Based on the conducted parametric study, the required axial and bending capacities of piles in different ranges of eccentricities can be reached using the combination of tube wall thickness and GFRP fiber percentages.

Keywords: pile design; fiber reinforced polymer; FRP; composite pile; bridge design; GFRP; glass fiber reinforced polymer

1. Introduction

One of the major concerns of using conventional steel, concrete, or wooden piles in bridge structures is their short-term deterioration causing structural failure. In the marine environment, where saltwater accelerates corrosion, traditional materials are prone to corrosion in splash and tidal areas. In the presence of moisture and oxygen, even concrete piles are susceptible to corrosion because of the existence of the steel bars inside the concrete. Several solutions have been presented in the past, such as using epoxy as a coating layer or galvanizing the steel member [1]; however, these approaches had unsatisfying outcomes for increasing the lifespan of steel materials in a corrosive environment [2]. In the long run, excessive use of steel and reinforced concrete materials for pile construction increases the demand for restoration and strengthening [3]. The short lifespan of these conventional materials can increase the cost of maintenance significantly. For instance, either replacing or repairing these piling systems costs more than one billion dollars annually in the U.S. [4]. Maintenance costs in Great Britain are also high, as the allocated budget for repairing bridges is roughly 500 million Euros per year (\$592,070,000) [5]. In contrast, fiber reinforced polymer (FRP) is resistant to corrosion compared to steel and other traditional materials. Furthermore, FRP piles can dissipate and absorb the impact energy of ships and other vessels, as well as serve as mooring points. Based on the highly acceptable performance of FRP materials for applications in marine engineering, using FRP materials in construction has gained

a reputation as a practical solution against corrosion, as well as to improve the durability of structural members in a marine environment. Moreover, FRP reinforcement is a more reliable replacement to steel reinforcement, as it enhances the strength of the structure member without adding considerable weight to the structure [6]. Therefore, fiberglass piles are considered as an ideal material for construction in the marine environment.

For the design of composite deep foundations in bridge structures, hybrid fiber-reinforced (FRP) materials have greater advantages, compared to non-hybrid materials. For instance, as a hybrid reinforcing method, glass fiber-reinforced polymer (GFRP) sheets have superior features regarding strength, tensile ratio, and stiffness-to-weight ratio. GFRP is both nonmagnetic and nonconductive, which is an advantage compared to traditional materials [7]. Furthermore, the constructability of GFRP is useful for structures which have complex shapes. In addition, these hybrid FRP polymers are more resistant to hazardous environments when exposed to saltwater, or even during destructive hurricanes. Therefore, in specific environmental conditions, such as coastal areas, replacing conventional pile members with GFRP composite piles considerably improves the lifespan of the constructed members against corrosion. Because they enhance the lifespan of the pile, GFRP piles also are deemed as a cost-effective alternative for traditional piles, as they increase the repair cycle of pile bridge foundations.

Analyzing the behavior of a strengthened structural member, such as its flexural capacity, deflection response, failure modes, moment redistributions, and ductility, are significant factors for developing accurate design methods and practical structures. Ductility is a critical factor in the construction process; for example, in statically indeterminate structures, it governs moment redistribution within plastic hinges. Redistribution of the moment in structural members ensures the full-capacity usage of the members, which is an essential factor when designing structures that are economical [8].

GFRP is considered a preferred material for enhancing the strength of piles, following methods such as near-surface-mounted and externally-bonded reinforcement techniques [3]. Developing the application of GFRP hybrid materials for use in construction enhances the ductility of the assembled structural members, as well as their flexural strength. Using epoxy resin for externally bonding GFRP sheets increases the strength of members during flexural loading.

An advantage of using hybrid FRP laminates, such as GFRP sheets, is their nonlinear stress-strain behavior [9]. This behavior results in enhancing both the ductility and strength of the members [10–12]. On the other hand, unlike steel, non-hybrid FRP sheets demonstrate linear stress behavior; in contrast, FRP adds to the flexural capacity of the member but reduces the ductility of the member significantly [8].

Despite increasing demands for the use of FRP materials, as an alternative method to replace traditional reinforcement techniques, the behavior of such hybrid materials as GFRP sheets have not been subject to extensive amounts of research. Moreover, the design and implementation methods of hybrid materials have not been sufficiently established in the guidelines such as EUROCOMP, CUR 96, and BD90/05 when compared to FRP materials. This study examined the behavior of hybrid fiberglass tubes filled with recycled material and concrete for use in deep foundations (piles). Many research studies have been conducted on the structural responses of recycled concrete material [13], [14,15]. In this study, fiberglass tubes were filled with concrete containing recycled materials, such as shredded and used tires, to determine if the use of recovered materials resulted in lowering construction costs in an environmentally friendly manner. In this way, seemingly worthless materials could be used as part of the construction process, without sacrificing natural resources or producing hazardous materials during the construction process.

Significant factors should be considered in the design of structural members, such as composite piles which are reinforced with FRP layers. Using the appropriate hybrid material—for example, GFRP, hybrid carbon, and glass-reinforced polymers (HCG), or carbon fiber reinforced polymers (CFRP)—is one of these important factors. As another reinforced hybrid option, using basalt fiber-reinforced polymer (BFRP) sheets is almost 15% less expensive than using GFRP materials, and with the same compressive strength as GFRP [16]. Moreover, the arrangement, thickness, and width, along with

the number of the designated layers, and compressive strength of the hybrid material affect the experimental outcomes.

Another important parameter is the shape of the reinforced materials, in that various circular or squared arrangements of the specimens may result in different outcomes. Some experimental research works have been performed on the performance of circular tubes using FRP material [17–22]. Hybrid FRP materials such as GFRP are composed of either bonded or embedded fibers in a matrix arrangement. This specific matrix pattern transfers structural loads within mediums and reinforces the fibers against environmental hazards. With this arrangement, the fibers mainly are designed to sustain structural loads [23].

Moreover, the direction of applied loads and the stiffness of a pile affect the results considerably. Based on the axial or lateral loading design criteria, the structure of the FRP tubes can be modified to enhance the strength capacities. For example, the tubes can be filled with concrete to increase their strength and stiffness. The filled tubes function as a permanent formwork that confines and protects the concrete. In addition, the tubes serve as flexural reinforcement for concrete by preventing local buckling of the tubes. Therefore, the considerable axial capacity and lateral strength of the FRP composite piles make them a reliable alternative to replace traditional piles.

2. Materials and Methods

This research studies the effect of using GFRP composite piles following the winding method on the capacity and durability of bridge structures. Full-scale test piles which are made of precast members were used for experiments. The test piles are reinforced in circular directions and containing concrete or recycled materials as fillers. A specific pattern is applied using the winding method. Polyester material, such as resin, is utilized to construct the GFRP fibers.

2.1. Material Properties

The GFRP tubes are made of E-glass epoxy with the yield tensile strength of 27,500 psi following the ASTM D638 code. The yield tensile elongation of the epoxy has a nominal unit value of 0.4 to 6.7% based on the ASTM D638 standard. The composite full-scale GFRP tubes used in this research are constructed using the filament winding fabrication technique. This technique is appropriate for circular hollow components and is applied in this research based on the cylindrical shape of the piles. This method can be performed quickly and is a cost-effective approach for laying the material. The conversion procedure of fiber to fabric is eliminated in this method which in respect decreased the amount of needed fiber material. Moreover, due to the straight predetermined pattern of fabricated fibers in this method, structural properties of the fibers, such as FRP or GFRP are matched with the direction of the applied loads.

The GFRP tubes are made of 7.5 mm structural wall thickness and the outer diameter of the test piles are between 227 mm and 241 mm. These GFRP tubes consist of three layers as inner, structural and protection laminates. In the test piles, fiber-oriented material is used with almost 40 degrees of longitudinal inclination from the horizontal axis of the pile. As is shown in Figure 1a, the GFRP tubes consist of three laminate layers which are asymmetrically rotated (+35/−86). The reinforces fibers orientated at 35° toward the longitudinal direction as they are oriented at 3° toward the hoop direction. Expansive additive materials in the tube enhanced the strength of the existing concrete against shrinkage and maintained the compression strength of the member. Regarding the used concrete mixture, three 150 mm × 300 mm cylinder samples were tested following the ASTM C39-2015 standard.

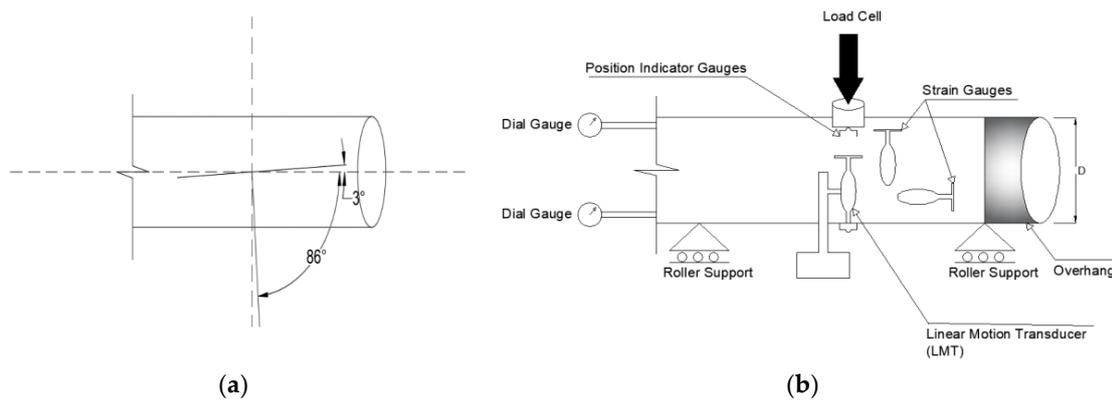


Figure 1. (a) Rotation of composite glass fiber-reinforced polymer (GFRP) fibers toward the longitudinal (35°) and hoop directions 3°, (left), (b) instrumentation of full-scale specimens using strain, dial and PI gauges along with Linear Motion Transducer (LMT) (right).

Figure 1b presents a schematic of the instrumenting used for conducting full-scale tests on the GFRP reinforced specimens. The strain gauges were set on the outer perimeter of the composite tubes to record hoop and longitudinal strain values. The midspan deflections were recorded using two 350 mm Linear Motion Transducers (LMTs). In addition, Dial Gauges were used to control small slips in the longitudinal direction between the composite tube and concrete. Two Position Indicator Gauges (PI Gauges) were installed in the midspan at both the top and bottom of the specimens to add more precision in measuring longitudinal displacements. The overhang region is designated for bending moment application during the tests.

2.2. Experimental Tests on GFRP Piles

The experiments are conducted on the full-scale GFRP reinforced piles. A full-scale pile test using GFRP material was built and used in the laboratory experiments to increase the accuracy of the test results. After determining the specific stiffness of the tested tube member, the sample's strength was calculated by applying axial-loading and moment-loading scenarios. The used GFRP tube is used for circumferential and longitudinal reinforcement of the test piles. The GFRP tubes are filled with recycled material. The structures of three different specimens were analyzed, and the ultimate capacities for loading and bending were measured. During the tests, the responses of the tubes under concentric and eccentric axial loading conditions are measured using column samples. The responses of the piles under bending loads are also measured for the beam samples. Table 1 shows the values and types of applied loadings. Purely bending load using beam samples (BE), the combination of bending load and axial load in compression using eccentric load on column samples (BE-AX), and purely axial load in compression applying concentric load on the column samples (AX) are shown in this table. Moreover, Table 1 illustrates the eccentricity of the compressive axial load (e), the length of beam sample spans (L), and the height of the sample columns under eccentric and concentric loading conditions (H). In addition, the ultimate measured values of axial compression load and the ultimate measured values bending moment are included in this table.

Table 1. Experimental data and specifications of specimens, including beams, concentrically and eccentrically loaded columns.

Test Pile ID	Tube Type	Eccentricity (mm)	Span Length/Height (m)	Axial Load in Failure (KN)	Moment Load in Failure (KNm)
BE 1-1	Tube 1	∞	4.50	0	112
BE-AX 1-1	Tube 1	647	1.60	198	176
BE-AX 2-1	Tube 1	322	1.60	326	144
BE-AX 3-1	Tube 1	239	1.60	312	126
BE-AX 4-1	Tube 1	144	1.60	427	237
BE-AX 5-1	Tube 1	54	1.60	344	117
AX-1-1	Tube 1	0	1.0	677	0
BE 1-2	Tube 2	∞	4.50	0	96
BE-AX 1-2	Tube 2	547	1.55	446	156
BE-AX 2-2	Tube 2	417	1.55	557	160
BE-AX 3-2	Tube 2	310	1.55	612	211
BE-AX 4-2	Tube 2	189	1.55	643	206
BE-AX 5-2	Tube 2	21	1.55	811	53
AX-1-2	Tube 2	0	0.97	901	0
BE 1-3	Tube 3	∞	4.50	0	116
BE-AX 1-3	Tube 3	733	1.75	288	136
BE-AX 2-3	Tube 3	522	1.75	401	255
BE-AX 3-3	Tube 3	319	1.75	522	274
BE-AX 4-3	Tube 3	199	1.75	622	144
BE-AX 5-3	Tube 3	71	1.75	848	202
AX-1-3	Tube 3	0	0.94	1002	0

BE: bending load, BE-AX: combined axial compression load and bending moment, AX: axial compression load.

Specifications of the GFRP Tubes

Three types of GFRP tubes are used in the experiments. Table 2 shows the mechanical properties of these GFRP which are labeled as T-1, T-2 and T-3. In addition, Table 2 presents specifications of these three GFRP tubes—such as outer diameters, Poisson ratio, compressive and tensile strength values of tubes. The orientation of the fibers in the tubes is comparable in that in each of the GFRP tubes, almost 60% of the fibers orientated at 35° and 40% at 86° with respect to the longitudinal direction. The GFRP reinforced pile members were designed following the winding method. Considering the longitudinal tension forces in the axial direction of the tested piles, and based on lamination theory, the failure modes of the GFRP piles were analyzed. For measuring the bending forces, four stations were controlled. Three geometrically identical beam specimens were used to evaluate the bending capacity of the piles. Based on the experiments of the beams, the total member responses were curvilinear; therefore, cracking could be omitted when considering higher amounts of loading strength under moment loading conditions.

Table 2. Tested Specifications for GFRP tubes.

GFRP Type	T-1	T-2	T-3
Average E_{Axial} , (GPa)	14.3	16.6	19.5
Average E_{Hoop} , (GPa)	15.2	17.3	21.4
Outer Thickness (mm)	4.31	4.87	5.24
Poisson Ratio	0.071	0.085	0.092
Tensile strength * (MPa)	178	201	263
Compressive strength * (MPa)	164	187	255
Diameter (mm)	227	236	241

* Tensile and Compressive Stresses were measured in the Longitudinal Direction.

2.3. Beam and, Column Specimens

Table 1 presents the details of the beam specimens and column specimens subjected to concentric and eccentric loads using GFRP tubes. BE 1-1, BE 1-2, and BE 1-3 beam specimens are made of the three types of the GFRP tubes, T-1, T-2, and T-3, as their specifications are shown in Table 2. The geometry of the three full-scale test beams was identical. The span of the test beams was 4.5 m and the distance between the applied loads was 1.2 m. Figure 2 shows the arrangement of the installed instrumentation such as for the full-scale piles reinforced with the GFRP composite tubes. Constant moment region instrumentation such as hoop and longitudinal strain gauges were used to measure the circumferential (hoop) and longitudinal displacements of these three beam specimens. A hydraulic actuator was used to measure the compressive strength of the specimens at a fixed deflection rate of 1.5 mm/min.

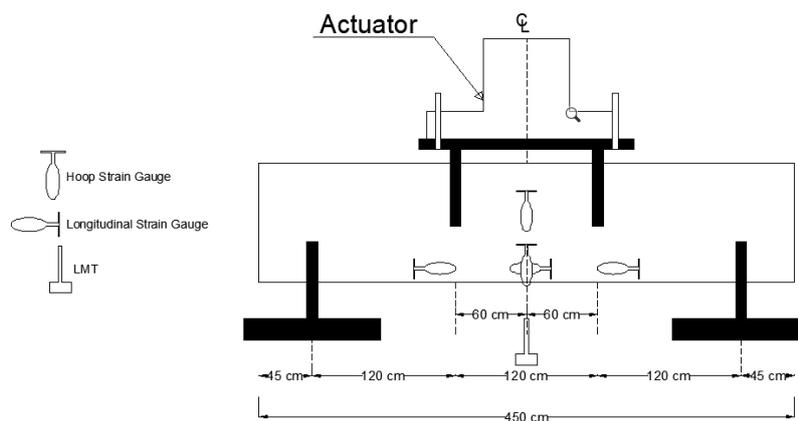


Figure 2. Instrumentation and beam test setup.

The displacement of the beam at the midspan and the amount of the load application is recorded during the tests. The ultimate bending capacity for each beam is recorded. The results are shown as moment load in failure in the Table 1. The goal here was to measure responses of the geometrically identical beams reinforced with three different types of the GFRP tubes, as is shown in the Table 2. The load-displacement behavior, load-deflection response, of the beam specimens at midspan is illustrated in Figure 3. The general responses of the beams are curvilinear before reaching the failing points. Moreover, in all three beam specimens, the ultimate load capacity was considerably greater than the calculated load for cracking the samples. Some minor data fluctuations occurred; however, they were insignificant due to the sample's calibration and initial measuring conditions [24].

Table 1 also provides specifications of the columns under a concentric compression load, which are mentioned as AX-1-1, AX-1-2 and AX-1-3. All these three full-scale column specimens have comparable geometry specifications. The height of these columns was almost 1 m. Ultimate axial and bending capacities of these full-scale column specimens under concentric loads are reported in Table 1. The average accumulated axial load-strain response of the columns is presented in Figure 4. The results were based on the mean value of three installed strain gauges to control the displacements in these columns. Figure 4 also delineated the comparison of the results with the idealistic axial-strain behavior following the lamination theory. Linear stress-strain behavior of the GFRP piles is simulated following a linear regression based on the results of this experimental study. The distribution of the forces in the GFRP tube along with concrete material was measured using numerical integration. The internal moment capacity of the pile was predicted at various strain levels using these calculated forces. The verification of the material is explained in the following section.

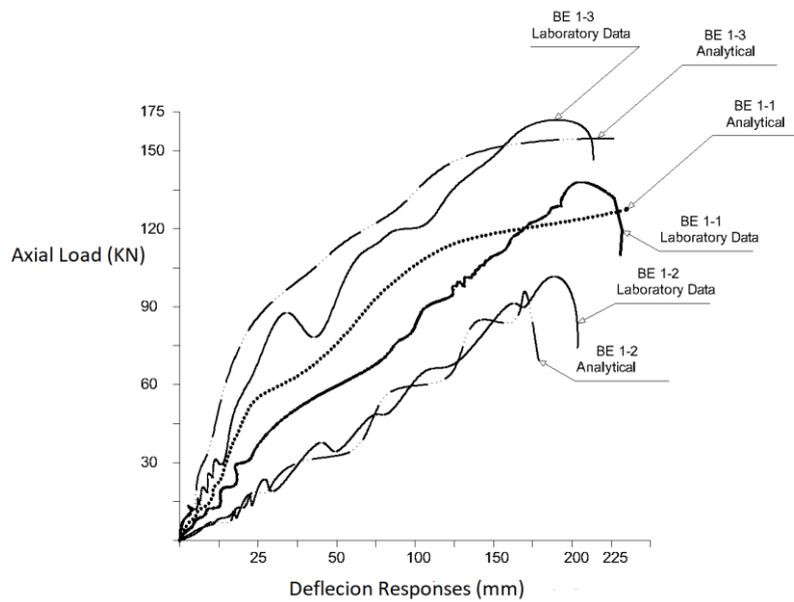


Figure 3. Axial compression load-deflection response of the test beam specimens.

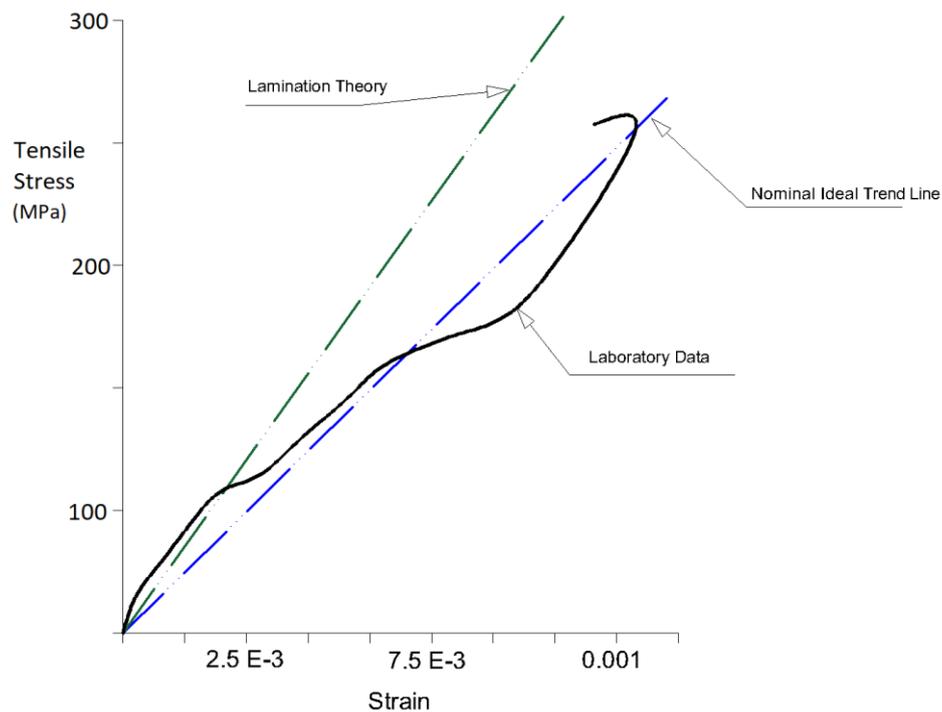


Figure 4. Comparison of axial stress–strain based on laboratory data, the lamination theory, and an ideal hypothetical line. The GFRP material properties are as shown in Table 2, compressive strength of the concrete in the pile: 30 MPa.

Furthermore, the specifications of three full-scale columns under the combination of axial compression load and bending moments are presented in Table 1 as BE-AX 1,2,3,4,5. Three types of GFRP reinforce tubes are implemented in these columns. For instance, BE-AX 2-1 is the second column under eccentric loads and reinforced with T-1 type of the GFRP tubes. The eccentricity of the applied loads and height of the test specimens are shown in Table 1. Rigid steel plates are installed at both ends of the column specimens and utilized to provide the test columns with five variations of eccentric loads during the test. The axial and moment load were applied on the bottom and top of the column

specimens as coupled forces. The measured ultimate axial and moment capacities of these full-scale columns are also reflected in Table 1. The ultimate axial compression load and ultimate moment load in the failure of the columns at the middle of columns' height are recorded in Table 1 for different eccentricity values. For the columns under eccentric loads, the ultimate axial capacity is measured from 198 to 848 KN, and the ultimate moment capacity of these three full-scale column specimens is ranged from 53 to 274 kNm. The ratio of eccentricity to the outer diameter (e/D) for the BE-AX Tube -1 columns that are reinforced with T-1 type of GFRP varies between 0.238 and 2.850. The ratio for the BE-AX Tube -2 columns with the presence of T-2 type of GFRP is ranged from 0.089 to 2.318. The ratio is also between 0.295 and 3.041 for the BE-AX Tube -3 column and the use of T-3 type of the GFRP tubes.

Circumferential, longitudinal and lateral deflection of the eccentrically loaded column specimens were recorded using three strain gauges during the test. Figure 5 delineates the resulted moment-curvature responses of the eccentrically loaded full-scale columns. This moment-curvature response of the composite GFRP tube filled with concrete was simulated using a modified strain compatibility and equilibrium concept. In this regard, the circular cross-section of the composite pile is modeled using divided horizontal layers. The GFRP reinforced tubes create a cylindrical geometric shape around the concrete.

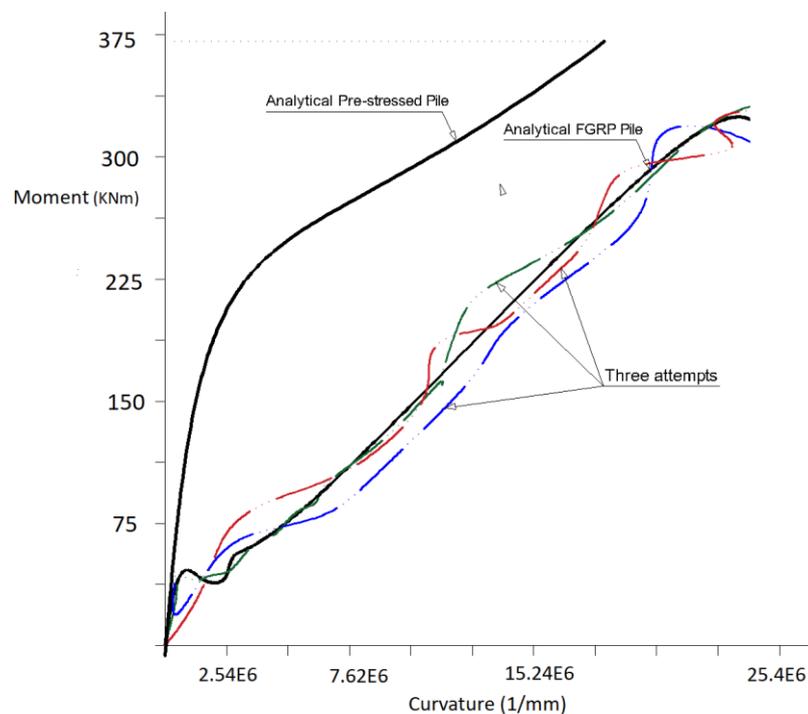


Figure 5. Moment-curvature analogy of eccentrically loaded column specimens reinforced with GFRP tubes compared to the analytical pre-stressed model.

3. Discussion and Results

Based on the laboratory data, and analysis of pile response, the curvature graph controlled based on the bending moment of the composite tubes. The responses of the tube members after cracks were determined. The overall slip between the recycled materials and the GFRP tubes is measured.

3.1. Material Verification

Material verification was controlled following the “coupon” testing methods and based on the lamination theory to calculate the maximum measured stiffness and strength capabilities of the GFRP members [25]. The first step was to test a rectangular-shaped strip layer sample. The actual strength

measurement of the tube had an error at the very end of both fixing locations because of the stress concentrations around those regions [26].

In the next procedure, steel tubes were used as a cover around the fiberglass tubes, along with resin to fill the empty voids. In this step, the GFRP coupons had a free (unfixed) length of 178 mm. After completion of the preparation stage, the GFRP samples at the fixed-end positions were tested under tension loading. Figure 4 illustrates the results of the accumulated strain and stress following the laboratory tests.

3.2. Response Evaluation of GFRP and Pre-Stressed Piles

As mentioned before, the full-scale composite GFRP piles are instrumented using strain gauges to measure the deflection at the middle of the height of the eccentrically loaded column specimen. The strain gauges are also used to record the strains of the extreme fibers under tension and compression, based on the applied constant bending moments on the specimens. The relative slip range of the GFRP tube in contact with the recycled material is measured at both top and bottom of the columns. The load application is conducted by controlling strokes and appropriate care of cushion. The average rate of the loading was 1.5 mm/min.

Figure 5 depicts the curvature-moment responses of the GFRP piles for the three geometrically similar eccentrically loaded column specimens. The crack moment, 43 kNm, is considerably small compared to the ultimate bending capacity of the specimens. An immediate drop in the bending capacity of the columns is recorded which is the result of the stroke control test after occurring the crack. An analytical comparison is conducted between the responses of the GFRP composite piles and pre-stressed piles filled with concrete. A prediction of curvature-moment response of the pre-stressed piles was calculated following the strain compatibility and equilibrium theory. Details of such an analytical model is available in the previous research studies [27]. The Ramberg–Osgood equation was used to simulate the relationship between strain and strain responses of the pre-stressed strands. To simulate the nonlinear stress-strain behavior of the concrete in the pile reinforced with these pre-stressed steel material, a generalized expression model by Popovics [28] is used. This predicted curvature-moment response of the pre-stressed concrete filled pile is shown in Figure 5 for analytical comparison purposes. ACI 318M-19 Standard and AASHTO LRFD bridge design specification limited the ultimate useable compressive strain to 0.003, for the conventional plain concrete with limited ductility [29,30]. Following these standards, the same ultimate maximum strain of the concrete is used in the prediction of the responses of the pre-stressed piles filled with concrete material [31].

The behavior of pile members in different loading scenarios is governed by type of the materials used for the construction of the piles. As a result, various composite materials considered in this research such as GFRP tubes, recycled and concrete materials provide the pile members with different strength and pile-deflection responses. Full-scale specimens provide this study with the opportunity to examine the response of such some composite pile members. Due to the various strengths of these materials, bridge design specifications recommend several types of design methods to deal with different reinforcement systems of pile members [32].

Based on the responses, analyses of the pile members were performed by comparing moment-curvature graphs [33]. First, the geometric characteristics of the GFRP filled with recycled materials were analyzed. A filled GFRP tube was stripped longitudinally and sampled. From the stress-strain data gleaned from the experimental test, which was semi-linear, the internal forces acting on the filled materials and the GFRP were evaluated by conducting a numerical analysis, as well as using regression on the resultant laboratory data, as is shown in Figure 5. Second, in order to develop the moment-curvature diagram, the calculated internal forces were used to anticipate the internal moments in various locations following the estimated strain data. Three tests were conducted to compare the lateral responses of the GFRP piles.

As is shown in Figure 5, when the internal moments reached the failure point, cracking occurred. At the cracking failure point, the moment capacity of the GFRP is decreased significantly following a

non-linear response. Before the cracking, the stiffness capacity of the GFRP tubes and conventional pile were almost identical. Since the GFRP piles were filled with recycled materials, as a replacement of corrosive steel for reinforcement of the pile, the occurrence of the cracks will not affect the lifespan of the members in the long term because of eliminating the agent of the corrosion.

3.3. Field Results on GFRP Piles, Parametric Study

As mentioned before, the use of full-scale test piles results in a more reliable outcome for analyzing the responses of the GFRP composite piles [25,34,35]. The capacities of GFRP composite piles were measured under axial loading. Installed strain gauges and accelerometers measured the member’s displacements for both longitudinal and lateral loadings. The lateral deflection and displacement of the pile, as well as the axial strain and displacement responses of the piles, were measured and analyzed. For further illustration of the effect of GFRP tubes on the axial and bending capacities of the piles, a parametric study is presented as follows:

In this parametric research, the effect of different percentages of fibers on the axial and bending resistances of a test pile is investigated. Furthermore, variations of thickness of the GFRP composite tubes in both longitudinal and hoop directions on pile capacities are studied.

In this research, A GFRP composite tube with 250 inner diameters and filled with 30 MPa concrete is constructed using E-glass epoxy with the yield tensile strength of 27,500 psi based on the ASTM D638 specifications. Three arrangements for the laminate structure of the GFRP tubes were selected. The implemented percentages of GFRP fiber tubes in the longitudinal and hoop directions are varied using 1:6, 1:1 and 6:1 ratios. The 1:6 ratio indicates that 60% of the GFRP fibers are orientated in the hoop directions to increase the confinement capacity of the tubes under axial compression loading. The 6:1 GFRP laminate has 60% of these fibers orientated in the longitudinal direction to enhance the bending capacity of the composite tubes. The 1:1 ratio defines an equivalent distribution of fiber percentages in both hoop and longitudinal directions. Each of these ratios in the structures of the laminates is tested with wall thicknesses (t) 5, 7.5 and 15 mm, which are in respect equal to the 8%, 12% and 24%, as pile reinforcement ratios (4t/D). An analytical model is used to develop the interaction diagram [25]. The combination of three different proportionate percentages and three different thickness values, a total of 9 cases, were analyzed.

Figure 6 shows the axial-moment load interaction curve diagrams based on the thickness and fiber percentage variables. The axial compression and bending moment capacities of the tubes are presented based on the diameter of the pile D and compressive strength of the concrete f'_c . In each diagram, three curves show the fiber proportionate ratios of the GFRP laminate structures based on the specified 4t/D ratios. The diagrams show that an improvement in longitudinal stiffness properties of the pile, for example from 1:6 to 6:1 fiber ratios, considerably adds to the moment capacity of the tubes in different thickness variations. In addition, increasing the GFRP tube thickness results in enhancing both axial and bending capacities. However, an increase in hoop stiffness, for instance from 6:1 to 1:6 fiber ratios is not necessarily increasing the pure axial capacity of the pile in compression for different thickness values. For example, for a 15 mm-thick GFRP tube, adding to the hoop stiffness is not increased the axial capacity of the pile. Although, for the tube with a thickness of 5 mm the increase of hoop stiffness results in enhancing the pure axial compression capacity. These outcomes for responses of the pile can be justified using the equations below [25]. In the Equations (1)–(3), P_{AX} is the ultimate axial capacity in interaction with the concrete P_C and the GFRP tube P_{GFRP} . The cross-section area of the concrete is shown as A_C and f'_{cc} represents the confined compressive strength of the concrete. E_f is the effective modulus elasticity and ϵ'_{ff} is the axial strain capacity of the tube at both ends.

$$P_{AX} = P_C + P_{GFRP} \tag{1}$$

$$P_C = A_C f'_{cc} \tag{2}$$

$$P_{GFRP} = A_f E_f \epsilon'_{ff} \tag{3}$$

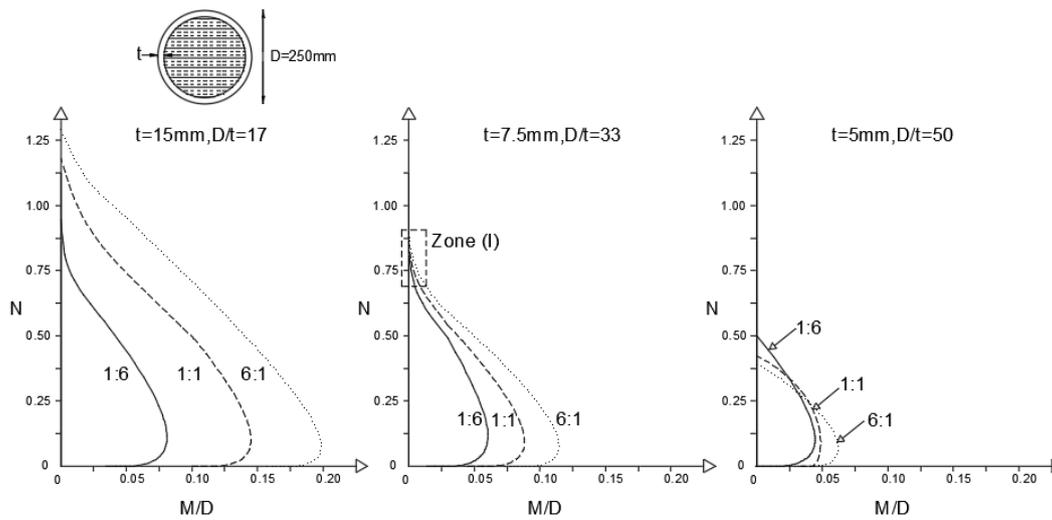


Figure 6. Axial load-bending moment interaction curves for GFRP composite tubes with different thickness values and fiber percentages.

The reduction of the hoop stiffness is shown by the decrease of the f'_{cc} in Equation (2). Therefore, the P_{AX} is reduced in Equation (1). P_{GFRP} is increased by increasing the longitudinal stiffness of the tube. For small variations in the thickness the rate of decrease of the P_C is more than the increasing rate of the P_{GFRP} . As a result, the ultimate axial compression load capacity, P_{AX} , is decreased. However, for large thickness values, the P_{AX} becomes greater due to the increasing rate of the P_{GFRP} . The decline in the rate of hoop stiffness does not considerably affect the P_{AX} for large thickness values. For the median values of the thicknesses, the reducing amount of the P_C happens at the same rate as the P_{GFRP} increment and consequently, the change rate of the P_{AX} is almost constant, as is presented in the Zone I of Figure 6 for the GFRP tube with 7.5 mm thickness ($D/t = 33$). For the larger wall thicknesses, D/t within 33 and 17, interaction curves for various structures of GFRP tubes have no intersection. For the smaller thickness values, D/t between 33 and 50, the interaction curves have points of intersection.

These intersection points affect the effectiveness of the design procedure for various eccentricity values. For instance, as shown in Figure 6, the curve attributed to the 6:1 ratio and with a relatively large eccentricity e_A , is tangent to the other two curves and acts as the envelope of the family curves.

Therefore, the 6:1 ratio is the most preferable fiber percentage for the design procedure compared to 1:6 and 1:1 ratios. On the other hand, the interaction curve related to the 1:6 ratio and with relatively small eccentricity e_C , is the envelope curve, compared to the other two curves. Therefore, the 1:6 is the most desired fiber proportion for the small eccentricity values. For the median eccentric values, e_B , all the three curves attributed to 1:6, 1:1, and 6:1 have comparable efficiency to be selected for the design procedure. As a result, the ultimate axial and bending capacities of the piles are directed by the combination of GFRP fiber percentages and the tube thickness values for different ranges of eccentrics.

3.4. Significance of the Research

This study evaluated the response of full-scale piles in experimental analysis. The piles were reinforced with three different laminate structures of GFRP tubes. The tests were performed for pure bending, the combination of axial compression load and bending moment, along with the pure axial compression loading conditions. GFRP composite tubes were reinforced in both circumferential and longitudinal directions. The study investigated the use of GFRP reinforced piles as an alternative to the piles reinforced with FRP piles. Compared to the traditional reinforcement methods or use of FRP tubes, the application of the GFRP tubes is a more cost-effective practice in large-scale constructions such as bridge piers and has a considerable environmental impact. A parametric study is presented following the experimental tests for both axial compression and bending load applications.

3.5. Conclusions

Following the experimental data analysis, the use of glass-fiber-reinforced polymer has many benefits for the design and implementation of pile structures in large-scale construction projects, such as bridge structures. The use of piles reinforced with GFRP material in bridge design results in increasing the durability of these deep foundations and decreasing their construction costs. The allocated expenditure for recovering and repairing pile structures in both North America and Europe exceeds \$1.5 billion dollars. Therefore, maintenance cost is a significant factor in the design of cost-effective structures. Using recycled materials as fillers in reinforced GFRP tubes decreases the total cost of production. In the past decade, using steel-reinforcement methods increased the cost of construction; however, developing structural piles with hybrid GFRP materials resulted in reducing the use of steel materials as reinforcing members. In addition, hybrid FRP materials, such as GFRP, enhance the anticipated lifespan of pile structures, even in such hazardous environments as oceans, where corrosion is one of the main concerns for the durability of these structures. Finally, these hybrid materials increase the anticipated strength capacity of the structures significantly.

The outcome of this research is based on a specific arrangement of GFRP layers, including their diameter, outer and inner thickness, and the degree of inclination from the longitudinal direction. Adjusting these specifications, as well as changing the material's properties—such as E_{Axial} , E_{Hoop} , and Poisson ratios—optimized the results. Based on the results from three full-scale samples, the deflection responses were linear in an axial loading condition before reaching the failure criteria. Since recycled material was used as filler inside the tubes, the long-term effect of cracking was negligible for high values of calculated strength, as well as under axial or lateral loadings. Some minor inconsistencies in such parameters as initial measurements or the calibration of samples could affect the outcomes.

Analyzing the internal forces of the GFRP tubes filled with recycled material showed the semi-linear behavior of the pile members, which resulted in increasing the total strength and ductility of the reinforced piles. The lateral responses of both the GFRP piles and pre-stressed piles showed comparable results, in that the effect of cracking under axial and lateral loadings was negligible.

A parametric study is conducted to investigate the effect of wall thickness and fiber percentages of the GFRP tubes on the axial and bending capacities of the piles. The structure of GFRP tubes, such as their thickness and ratios of the implemented GFRP in the pile considerably affects the axial-moment interaction curves of the piles. The T-2 type GFRP tube with higher hoop elastic modulus, 17.3 Gpa and relatively low Poisson's ratio 0.085 has more confinement strength compared with T-1 and T-3 tubes with lower hoop modulus of elasticity values. Furthermore, the axial capacity of the tubes is changed due to higher GFRP fiber ratios in the hoop direction for small thickness values. However, the bending capacity of the tubes is governed by both thin and thick wall structures tubes for higher GFRP fiber ratios in the longitudinal direction. The increase rate of axial capacity for the GFRP with more thickness values tubes is higher in the longitudinal direction compared to the hoop direction. Furthermore, the effect of axial capacity is higher than the confinement capacity in tubes with lower thickness values. The required axial and bending resistance capacities of piles in different ranges of eccentricities can be met using the combination of tube wall thickness and GFRP fiber percentages following the curve interaction diagrams.

Further studies are recommended to investigate the developing of more reliable methods using full-scale test specimens with different laminate structures, various percentages of GFRP material along with using the tubes in different directions in both longitudinal and hoop directions. Furthermore, the effects of using other materials such as basalt fiber-reinforced polymer, as an alternative for GFRP material, could be investigated for more cost-effective design and implementation of piles.

Author Contributions: Conceptualization, V.F.; methodology, V.F.; writing—original draft preparation, V.F., M.K.; writing—review and editing, M.K.; supervision, M.K. All authors have read and agreed to the published version of the manuscript.

Funding: The publication fees for this article were supported by the UNLV University Libraries Open Article Fund. This research received no additional funding.

Conflicts of Interest: The authors declare no conflict of interest.

References

- Clarke, J.L. Fiber-Reinforced Plastic Reinforcement for Concrete. *Concr* **1999**, *33*, 15–16.
- Keesler, R.J.; Powers, R. *Corrosion of Epoxy Coated Rebars Keys Segmental Bridge -Monroe County, Report No.88-8A*; Corrosion Research Laboratory, Florida Department of Transportation, Materials Office: Gainesville, FL, USA, 1988.
- Oh, M.H.; Hong, S.N.; Kim, T.W.; Cui, J.; Park, S.K.P. Experimental Study on Deformation Recovery and Residual Strength of FRP RC Beams. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering (CICE 2010), Beijing, China, 27–29 September 2010.
- Lampo, R. *Federal Interest Gives Recycled Plastic Lumber a Leg Up*; ASTM: West Conshohocken, PA, USA, 1996.
- Broomfield, J.P.; Davies, K.; Hladky, K. The use of permanent corrosion monitoring in new and existing reinforced concrete structures. *Cem. Concr Compos.* **2002**, *24*, 27–34. [[CrossRef](#)]
- Tharmarajah, G.; Taylor, S.E.; Robinson, D.; Cleland, D.J. Arching Action in Laterally Restrained GFRP Reinforced Slabs. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering, Beijing, China, 27–29 September 2010.
- Panda, K.C.; Barai, S.V.; Bhattacharyya, S.K. Influence of Transverse Steel on the Performance of RC T-Beams Strengthened in Shear with GFRP Strips. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering, Beijing, China, 27–29 September 2010.
- Akbarzadeh, H.; Maghsoudi, A.A. Akbarzadeh, H.; Maghsoudi, A.A. Flexural Strengthening of RC Continuous Beams Using Hybrid FRP Sheets. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering, Beijing, China, 27–29 September 2010.
- Belarbi, A.; Chandrashekhara, K.; Watkins, S.E. Performance Evaluation of Fiber Reinforced Polymer Reinforcing bar Featuring Ductility and Health Monitoring Capability. In Proceedings of the Fourth International Symposium on Fiber Reinforced Polymers (FRP) for Reinforced Concrete Structures, Baltimore, MD, USA, 21 November 1999. ACI SP 188–29: 1–12.
- Xiong, G.J.; Jiang, X.; Liu, J.W.; Chen, L. A way for preventing tension delamination of concrete cover in midspan of FRP strengthened beams. *Constr. Build. Mater.* **2007**, *21*, 402–408. [[CrossRef](#)]
- Xiong, G.J.; Yang, J.Z.; Ji, Z.B. Behavior of reinforced concrete beams strengthened with externally bonded hybrid carbon fiber–glass fiber sheets. *J. Compos. Constr. ASCE* **2017**, *21*, 275–278. [[CrossRef](#)]
- Hosny, A.; Shaheen, A.; Abdelrahman, A.; Elafandy, T. Performance of reinforced concrete beams strengthened by hybrid FRP laminates. *Cem. Concr. Compos.* **2006**, *28*, 906–913. [[CrossRef](#)]
- Ignjatović, I.S.; Marinković, S.B.; Tošić, N. Shear behaviour of recycled aggregate concrete beams with and without shear reinforcement. *Eng. Struct.* **2017**, *141*, 386–401. [[CrossRef](#)]
- Fathifazl, G.; Razaqpur, A.G.; Isgor, O.B.; Abbas, A.; Fournier, B.; Foo, S. Shear capacity evaluation of steel reinforced recycled concrete (RRC) beams. *Eng. Struct.* **2011**, *33*, 1025–1033. [[CrossRef](#)]
- Silva, R.V.; De Brito, J.; Dhir, R.K. Comparative analysis of existing prediction models on the creep behaviour of recycled aggregate concrete. *Eng. Struct.* **2015**, *100*, 31–42. [[CrossRef](#)]
- Serbescu, M.; Guadagnini, K.P. Basalt FRPs for Strengthening of RC Members. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering, Beijing, China, 27–29 September 2010.
- Fam, A.; Cole, B. Tests on reinforced-concrete filled, fiber reinforced polymer circular tubes of different shear spans. *Can. J. Civ. Eng.* **2007**, *34*, 311–322. [[CrossRef](#)]
- Zhu, Z.; Ahmad, I.; Mirmiran, A. Effect of column parameters on axial compression behavior of concrete-filled FRP tubes. *Adv. Struct. Eng.* **2005**, *8*, 443–449. [[CrossRef](#)]
- Ahmad, I.; Zhu, Z.; Mirmiran, A. Behavior of short and deep beams made of concrete-filled fiber reinforced polymer tubes. *J. Compos. Constr.* **2008**, *12*, 102–110. [[CrossRef](#)]
- Fam, A.; Son, J.K. Finite element modeling of hollow and concretefilled fiber composite tubes in flexure: Optimization of partial filling and a design method for poles. *Eng. Struct.* **2008**, *30*, 2667–2676. [[CrossRef](#)]
- Shao, Y.; Mirmiran, A. Control of plastic shrinkage cracking of concrete with carbon fiber-reinforced polymer grids. *J. Mater. Civ. Eng.* **2007**, *19*, 441–444. [[CrossRef](#)]
- Shao, Y.; Mirmiran, A. Experimental investigation of cyclic behavior of concrete-filled fiber reinforced polymer tubes. *J. Compos. Constr.* **2005**, *9*, 263–273. [[CrossRef](#)]

23. Vatani Oskouei, A.; Pirgholi Kivi, M.; Taghipour Boroujeni, S. Effect of CFRP and GFRP Confinement on Behavior of Square Lightweight Concrete Specimens. In Proceedings of the 5th International Conference on FRP Composites in Civil Engineering, Beijing, China, 27–29 September 2010.
24. Fam, A.Z.; Flisak, B.; Rizkalla, S. Experimental and Analytical Investigations of Beam-Column Behavior of Concrete-Filled FRP Tubes. *ACI Struct. J.* **2003**, *100*, 499–509.
25. Fam, A.Z.; Flisak, B.; Rizkalla, S. Precast Piles for Route 40 Bridge in Virginia Using Concrete-Filled FRP Tubes. *PCI J.* **2003**, *48*, 32–45. [[CrossRef](#)]
26. ACI Committee 318. *Building Code Requirements for Structural Concrete (ACI 318M-02) and Commentary (318 RM-02)*; American Concrete Institute: Farmington Hills, MI, USA, 2002.
27. Fam, A.Z. *Concrete-Filled Fiber Reinforced Polymer Tubes for Axial and Flexural Structural Members*; University of Manitoba: Winnipeg, MB, Canada, 2000.
28. Mitchell MPCD. *Prestressed Concrete Structures*; Prentice Hall: Englewood Cliffs, NJ, USA, 2001.
29. ACI 318 *Building Code Requirements for Structural Concrete (ACI 318M-19) and Commentary (318 RM-19)*; Farmington Hills, MI, USA, 2019; Available online: https://www.techstreet.com/standards/aci-318m-19?product_id=2094242#jumps (accessed on 1 February 2020).
30. AASHTO. *AASHTO LRFD Bridge Design Specifications*, 7th ed.; American Association of State Highway and Transportation Officials: Washington, DC, USA, 2014; Available online: <https://www.transportation.org> (accessed on 3 January 2020).
31. Kaka, V.B.; Kim, J.; Chao, S-H. Formulating Constitutive Stress-Strain Relations for Flexural Design of Ultra High—Performance Fiber-Reinforced Concrete. In Proceedings of the First International Interactive Symposium on UHPC, Iowa State University, Des Moines, IA, USA, 18–20 July 2016.
32. Committee on Pre-Stressed Concrete Piling. Recommended Practice for Design, Manufacture, and Installation of Pre-Stressed Concrete Piling. *PCI J.* **1993**, *38*, 403–414.
33. Daniel, I.M.; Ishai, O. *Engineering Mechanics of Composite Materials*; Oxford University Press: New York, NY, USA, 1994.
34. Fam, A.Z.; Flisak, B.; Rizkalla, S. Experimental and Analytic Modeling of Concrete-Filled Fiber-Reinforced Polymer Tubes Subjected to Combined Bending and Axial Loads. *ACI Struct. J.* **2003**, *100*, 499.
35. Pando, M.; Filz, G.; Hoppe, E.; Ealy, C.; Muchard, M. Performance of a Composite Pile in a Full Scale Statnamic Load Testing Program. In Proceedings of the Fifty-Third Canadian Geotechnical Conference, Montreal, QC, Canada, 2000; Volume 1, pp. 909–916.



© 2020 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).